SJIF Impact Factor 2022: 8.197 | ISI I.F. Value:1.241 | Journal DOI: 10.36713/epra2016

ISSN: 2455-7838(Online)

EPRA International Journal of Research and Development (IJRD)

Volume: 7 | Issue: 5 | May 2022

- Peer Reviewed Journal

PERFORMANCE EVALUATION OF R.C SEISMIC STRUCTURE BY CONSIDERING EFFECTS OF JOINTS FLEXIBILITY

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ABSTRACT

Reinforced concrete (RC) buildings designed before the mid-1970s may have serious structural deficiencies and are considered substandard according to current seismic design criteria. Specifically, the failure of the beam-column joints has been the cause of building collapse in many recent earthquakes worldwide. This report evaluates the seismic performance of beam column joints with three different details of beam and beam-column joint reinforcement. This work shows that the comparison study of SMRF and OMRF. It carried out to observe the difference in behaviour of buildings.

KEYWORDS - Pushover analyasis, Capacity spectrum curves, base shear, displacement, plastic hinge.

I. INTRODUCTION

Reinforced concrete (RC) is a composite structural material that combined by steel and concrete. Concrete with its compressive strength and steel with its strong tension strength have formed RC material. This results in high shear and bondstress demands in the joint, which in turn affects the overall performance of the moment frame. The compressive stresses were covered by concrete and tensile stresses were covered by steel in the structures was revealed RC materials.

II. RESEARCH OBJECTIVES

- To evaluate the behaviour of structure under different joint flexibility.
- To examine estimation of optimum rigidity factor.
- Analyse of beam column joint behaviour.

III. METHODOLOGY

A pushover analysis is performed by subjecting a structure to a monotonically increasing pattern of lateral loads, representing the inertial forces which would be experienced by the structure when subjected to ground shaking. Under incrementally increasing loads various structural elements may yield sequentially. Consequently, at each event, the structure experiences a loss in stiffness. Using a pushover analysis, a characteristic non-linear force displacement relationship can be determined

Analysis

Beams and columns were modelled as frame elements available in SAP 2000, with the central lines joined at nodes. Beam-column joints are considered as rigid beam-column joints and these are modelled by givingend offsets at the joints.

Analysis Output

The main output of pushover analysis is in the form of base shear versus roof displacement curve called pushover curves. This capacity curve is generally constructed to represent first mode response of the structure assuming that fundamental mode of vibration is predominant.

Effects of Plastic Hinge

The plastic hinge formation predicted by the various pushover methods was the same as that predicted by the nonlinear dynamic analyses .The inclusion in the analyses of the strain hardening effect did not delay the occurrence of the first hinge with respect to the EPP model but it did delay the occurrence of the mechanism's formation. The development of the plastic hinges predicted by both nonlinear dynamic analyses and pushover analyses. Creating basic computer model using graphical interface of SAP-2000The program includes several built in default hinge properties that are based on average value from ATC-40 for concrete member FEMA-356 for steel. These built in properties can be useful for preliminary analysis, but user-defined properties are recommended for final analysis.



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Fig- Nonlinear behavior of member



Fig- Yield rotation for concrete & steel

Default Nonlinear Hinge Properties For Beam

placement	Control Parameters -			
				. Iype
Point	Moment/SF	Rotation/SF		Moment · Rotation
E	-0,2	-0,025		C. Moment - Curvature
D+	-0,2	-0,015	_	
C-	-1,1	-0,015		Hinge Length
B-	- 1	0		Relative Length
A	0	0		
В	1,	0,		Hysteresis Type And Parameters
С	1.1	0.015		I I I I I I I I I I I I I I I I I I I
D	0,2	0,015	Gummetric	Hysteresis Type Isotropic 💌
F	0.2	0.026	. IA shumenc	
.oad Carryin	ng Capacity Beyond I To Zero spolated	Point E		No Parametes Are Hequired For This Hysteresis Type
oad Canyin	o.2 ng Capacity Beyond I To Zero apolated foment and Rotation eld Moment Mom	Point E Positive vent SF stion SF 1.	e Negative	No Farancies Xie Required for The Hystoresis Type
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Load Carryin C Drops C Is Extr Scaling for I Use Yi (Steel Acceptance	u.2 ng Capacity Beyond I To Zero apoleted Koment and Rotation eld Rotation Rota Digiests Only) I criteria (Plastic Rota vidate Occupancy	Point E Positive Nent SF Positive Posit	Negative Negative Negative	No Farancies Xie Required for The Hystoresis Type
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Load Carryin C Drops C Is Extr Scaling for I Use YI (Steel) Acceptance Immediate Life Colla	u.2 ng Capacity Beyond I To Zero apoleted Moment and Rotation ekil Rotation Rota Disecto Dn(y) r Criteria (Plastic Rot visita Occupancy Safety pse Prevention	0.025 Point E Point SF non SF 1. ation SF 9.0005 0.012 0.015	Negative Negative Negative	No Feranders Ale Required For The Hypothesia Type

Fig: Hinge Properties For Beam

For Column

Table 6-7	Mod Rein	leling Paran forced Con	c	ters and ete Bear	Numerica ms	al Acceptane	ce	Criteria	for Nonl	inear Pro	cedures-	-		
				Modeling Parameters ³				Acceptance Criteria ³						
								Plastic Rotation Angle, radians						
$1.0 \qquad \qquad$								Performance Level						
				Plastic Rotation Angle, radians		Residual Strength Ratio			Component Type					
									Primary		Secondary			
Conditions				а	b	c		ю	LS	CP	LS	CP		
i. Beams controlled by flexure ¹														
$\frac{\rho - \rho'}{\rho_{bal}}$	Trans. Reinf. ²	$\frac{V}{b_w d_s \int f_c}$					Ī							
≤ 0.0	С	≤ 3	t	0.025	0.05	0.2	T	0.010	0.02	0.025	0.02	0.05		
≤ 0.0	С	≥6	T	0.02	0.04	0.2	T	0.005	0.01	0.02	0.02	0.04		
≥ 0.5	С	≤ 3	T	0.02	0.03	0.2	T	0.005	0.01	0.02	0.02	0.03		
≥ 0.5	С	≥6	T	0.015	0.02	0.2	T	0.005	0.005	0.015	0.015	0.02		
≤ 0.0	NC	≤ 3	Γ	0.02	0.03	0.2		0.005	0.01	0.02	0.02	0.03		
≤ 0.0	NC	≥6	Γ	0.01	0.015	0.2		0.0015	0.005	0.01	0.01	0.015		
≥ 0.5	NC	≤ 3	Γ	0.01	0.015	0.2		0.005	0.01	0.01	0.01	0.015		
≥ 0.5	NC	≥6	Γ	0.005	0.01	0.2		0.0015	0.005	0.005	0.005	0.01		

Fig: Hinge Properties For Column

CONCLUSIONS

- 1. From above observations we can conclude that inaccurate modeling of joint stiffness also results in wrong prediction of seismic behavior of structure and failure of structural element may result in such buildings where joint rigidity is not taken in account structure during earthquake.
- 2. The current study highlighted that joint flexibility is essential for simulating existing RC structures constructed in Iran before the 1970s with non-seismic joint detailing and conventional analyses (rigid joint assumption) may not reflect the realistic responses of those types of RC structures under earthquake loading.
- 3. Plastic hinge length expression typically gives the hinge length as a proportion of either the member length or the member width. In reality the plastic hinge length is a function of member depth and length, as well as the diagonal shear crack angle.
- 4. The study of reinforced concrete columns clearly demonstrates the significance of plastic hinge behavior in its contribution to column failure. For fixed columns, a fully formed hinge releases the boundary constraints and enables the member to continue to act as though it were a simple support system. The final hinge to develop in a fixed column, or the only one to do so in simply supported column, provides the ultimate failure mechanism around which the column will invariably collapse under extreme forces.

Scope for Future Work

1. Experimental investigation on the behaviour of beam when it is semi- rigidly connected with column.

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2. Further research needs to establish the theoretical model for semi-rigidly connected continuous beam.

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